

Lecture 8: Sliding Mode DNN Control for Mechanical Systems

Plan of presentation

- Optimization of Attractive ellipsoid
- Feedback design
- Taking into account the PC-motor as an activating device
- How calculate derivatives on-line: super-twist differentiator

Attractive ellipsoid minimization

Problem

To minimize the Attractive Ellipsoid we need to resolve the following optimization with Nonlinear Matrix Constraints:

$$\operatorname{tr} \left\{ \frac{\alpha}{\varepsilon c_0} \begin{bmatrix} P_1 & 0_{n \times n} \\ 0_{n \times n} & P_2 \end{bmatrix} \right\} \rightarrow \max_{P_1 > 0, P_2 > 0, A, L, W_0^*, \alpha > 0, \varepsilon > 0}$$

subject to the matrix constraint

$$S := \begin{bmatrix} (\alpha - \varepsilon) P_1 & & & & \\ +2\varepsilon c_1 I_{n \times n} & P_1 - P_2 LC & & 0_{n \times n} & 0_{n \times n} \\ & \alpha P_2 + P_2 A + A^T P & & & \\ P_1 - C^T L^T P_2 & -P_2 LC - C^T L^T P_2 & & P_2 W_0^* & P_2 \\ & +2\varepsilon c_2 I_{n \times n} & & & \\ & (W_0^*)^T P_2 & & -\varepsilon I_{n \times n} & 0_{n \times n} \\ 0_{n \times n} & & & & \\ 0_{n \times n} & P_2 & & 0_{n \times n} & -\varepsilon I_{n \times n} \end{bmatrix} \leq 0$$

Necessary condition to fulfil NMI

Fact

One of necessary requirements to fulfil NMI is

$$(\alpha - \varepsilon) P_1 + 2\varepsilon c_1 I_{n \times n} \leq 0$$

or equivalently

$$\left. \begin{array}{l} \varepsilon > \alpha, \\ P_1 \geq 2 \frac{\varepsilon c_1}{\varepsilon - \alpha} I_{n \times n} \end{array} \right\}$$

(1)

Representation of the optimization aim

$$\operatorname{tr} \left\{ \frac{\alpha}{\varepsilon c_0} \begin{bmatrix} P_1 & 0_{n \times n} \\ 0_{n \times n} & P_2 \end{bmatrix} \right\} = \frac{\alpha}{\varepsilon c_0} (\operatorname{tr} \{P_1\} + \operatorname{tr} \{P_2\})$$
$$\rightarrow \max_{P_1 > 0, P_2 > 0, A, L, W_0^*, \alpha > 0, \varepsilon > 0}$$

or equivalently,

$$\operatorname{tr} \left\{ \left(\frac{\alpha}{\varepsilon c_0} \begin{bmatrix} P_1 & 0_{n \times n} \\ 0_{n \times n} & P_2 \end{bmatrix} \right)^{-1} \right\} = \frac{\varepsilon c_0}{\alpha} (\operatorname{tr} \{P_1^{-1}\} + \operatorname{tr} \{P_2^{-1}\})$$
$$\rightarrow \min_{P_1 > 0, P_2 > 0, A, L, W_0^*, \alpha > 0, \varepsilon > 0}$$

NMI as LMI in new variables

Introduce new variables

$$X_1 := P_1, X_2 := P_2, Y := P_2 A, Z := P_2 L, H := P_2 W_0^*$$

and use the Schur's complement obtain the following equivalent representation:

$$0 < P_1^{-1} = X_1^{-1} \leq Q_1 \Leftrightarrow \begin{bmatrix} Q_1 & I_{n \times n} \\ I_{n \times n} & X_1 \end{bmatrix},$$

$$0 < P_2^{-1} = X_2^{-1} \leq Q_2 \Leftrightarrow \begin{bmatrix} Q_2 & I_{n \times n} \\ I_{n \times n} & X_2 \end{bmatrix}$$

NMI as LMI in new variables: problem formulation

Problem

$$\frac{\varepsilon c_0}{\alpha} (\text{tr} \{Q_1\} + \text{tr} \{Q_2\}) \rightarrow \min_{X_1 > 0, X_2 > 0, Y, Z, Q_1 > 0, Q_2 > 0, \alpha > 0, \varepsilon > 0}$$

subject to the LMI constraints

$$\begin{aligned}
 & \begin{bmatrix} Q_1 & I_{n \times n} \\ I_{n \times n} & X_1 \end{bmatrix} > 0, \quad \begin{bmatrix} Q_2 & I_{n \times n} \\ I_{n \times n} & X_2 \end{bmatrix} > 0, \\
 S = & \begin{bmatrix} -(\varepsilon - \alpha) X_1 & X_1 - ZC & 0_{n \times n} & 0_{n \times n} \\ +2\varepsilon c_1 I_{n \times n} & \alpha X_2 + Y + Y^T & & \\ X_1 - C^T Z^T & -ZC - C^T Z^T & H & X_2 \\ & +2\varepsilon c_2 I_{n \times n} & & \\ 0_{n \times n} & H^T & -\varepsilon I_{n \times n} & 0_{n \times n} \\ 0_{n \times n} & X_2 & 0_{n \times n} & -\varepsilon I_{n \times n} \end{bmatrix} \leq 0
 \end{aligned} \tag{2}$$

Recuperation of original variables

If the solution of the optimization problem (2) is

$$X_1^* > 0, X_2^* > 0, Y^*, Z^*, Q_1^* > 0, Q_2^* > 0, H^*, \varepsilon^* > \alpha^* > 0,$$

then the the original parameters of the DNNO are as follows:

$$\begin{aligned} P_1^* &= X_1^*, P_2^* = X_2^*, A^* = (X_2^*)^{-1} Y^*, \\ L^* &= (X_2^*)^{-1} Z^*, W_0^* = (X_2^*)^{-1} H^*, \end{aligned}$$

and learning law becomes to be as

$$\begin{aligned} \dot{W}_{0,t} &= -\frac{\alpha^*}{2} (W_{0,t} - W_0^*) - \varepsilon^* \Lambda^{-1} (W_{0,t} - W_0^*) \varphi(\hat{q}_{1,t}) \varphi^\top(\hat{q}_{1,t}) \\ &\quad - \frac{\varepsilon^* \rho_t (W_{0,t} - W_0^*)}{\text{tr}\{(W_{0,t} - W_0^*)^\top \Lambda (W_{0,t} - W_0^*)\}}, \end{aligned}$$

$$\left. \begin{aligned} \frac{d}{dt} \hat{q}_{1,t} &= \hat{q}_{2,t}, \\ \frac{d}{dt} \hat{q}_{2,t} &= f_{NN}^* (\hat{q}_{1,t}, \hat{q}_{2,t}) + u_t, \end{aligned} \right\} \quad (3)$$

where

$$\left. \begin{aligned} f_{NN}^* (\hat{q}_{1,t}, \hat{q}_{2,t}) &= A^* \hat{q}_{2,t} + L^* \left[y_t - C \begin{pmatrix} \hat{q}_{1,t} \\ \hat{q}_{2,t} \end{pmatrix} \right] + W_{0,t} \varphi (\hat{q}_{1,t}) \\ &\quad \text{with Learning Law} \\ \dot{W}_{0,t} &= -\frac{\alpha^*}{2} (W_{0,t} - W_0^*) - \varepsilon^* \Lambda^{-1} (W_{0,t} - W_0^*) \varphi (\hat{q}_{1,t}) \varphi^\top (\hat{q}_{1,t}) \\ &\quad - \frac{\varepsilon^* \rho_t (W_{0,t} - W_0^*)}{\text{tr} \{ (W_{0,t} - W_0^*)^\top \Lambda (W_{0,t} - W_0^*) \}}, \end{aligned} \right\}$$

Feedback design

For DNNO-tracking error $\Delta_t = \hat{q}_{1,t} - q_{1,t}^* \in R^{2n}$ and for the Lyapunov function $V_t = \frac{1}{2} \Delta_t^T \Delta_t$ we have

$$\begin{aligned} \dot{V}_t &= \Delta_t^T \dot{\Delta}_t = \Delta_t^T P \left(\frac{d}{dt} \hat{q}_{1,t} - \dot{q}_{1,t}^* \right) = \\ \Delta_t^T (\hat{q}_{2,t} - \dot{q}_{1,t}^*) &= \Delta_t^T \left(\int_{\tau=0}^t f_{NN}^* (\hat{q}_{1,\tau}, \hat{q}_{2,\tau}) d\tau + \int_{\tau=0}^t u_\tau d\tau - \dot{q}_{1,t}^* \right) \end{aligned}$$

Select u_τ satisfying

$$\int_{\tau=0}^t f_{NN}^* (\hat{q}_{1,\tau}, \hat{q}_{2,\tau}) d\tau + \int_{\tau=0}^t u_\tau d\tau - \dot{q}_{1,t}^* = -\alpha_0 \Delta_t, \quad \alpha_0 > 0$$

or, equivalently,

$$f_{NN}^* (\hat{q}_{1,t}, \hat{q}_{2,t}) + u_t - \dot{q}_{2,t}^* = -\alpha_0 \dot{\Delta}_t = -\alpha_0 (\hat{q}_{2,t} - \dot{q}_{2,t}^*),$$

$$u_t = -\alpha_0 (\hat{q}_{2,t} - \dot{q}_{2,t}^*) - f_{NN}^* (\hat{q}_{1,t}, \hat{q}_{2,t}) + \dot{q}_{2,t}^*.$$

Feedback with DC-motor as actuator

If we take into account that

$$u_t := - \int_{\tau=t_0}^t \tilde{v}_{a\tau} d\tau,$$

$$\tilde{v}_{at} = \dot{u}_t = -\alpha_0 \left(\frac{d}{dt} \hat{q}_{2,t} - \dot{q}_{2,t}^* \right) - \frac{d}{dt} f_{NN}^* (\hat{q}_{1,t}, \hat{q}_{2,t}) + \ddot{q}_{2,t}^*,$$

(4)

then the motor-voltage v_{at} will be

$$\begin{aligned} v_{at} &= -R_a K_a^{-1} W^{-1} \int_{\tau=t_0}^t \tilde{v}_{a\tau} d\tau + K_e W^T \hat{q}_{2,t} + L_a K_a^{-1} W^{-1} \tilde{v}_{at} = \\ &R_a K_a^{-1} W^{-1} \left[-\alpha_0 (\hat{q}_{2,t} - q_{2,t}^*) - f_{NN}^* (\hat{q}_{1,t}, \hat{q}_{2,t}) + \dot{q}_{2,t}^* \right] + K_e W^T \hat{q}_{2,t} \\ &+ L_a K_a^{-1} W^{-1} \left[-\alpha_0 \left(\frac{d}{dt} \hat{q}_{2,t} - \dot{q}_{2,t}^* \right) - \frac{d}{dt} f_{NN}^* (\hat{q}_{1,t}, \hat{q}_{2,t}) + \ddot{q}_{2,t}^* \right] \end{aligned}$$

How calculate derivatives on-line: super-twist differentiator

The problem consists in estimating the *first derivative* of a signal $\phi(t)$ based on its noisy measurement

$$y(t) = \phi(t) + \eta(t).$$

Only two *assumption* will be made:

- the second derivative $\ddot{\phi}(t)$ of the base signal $\phi(t)$ is uniformly bounded by a known constant L , i.e.,

$$|\ddot{\phi}(t)| \leq L,$$

- the measurement noise $\eta(t)$ is uniformly bounded by δ , i.e.

$$|\eta(t)| \leq \delta.$$

Super-twist differentiator

Setting

$$x_1(t) := \phi(t), \quad x_2(t) := \dot{\phi}(t),$$

the problem is transformed into the design of an observer for the system

$$\left. \begin{aligned} \dot{x}_1(t) &= x_2(t), \quad \dot{x}_2(t) = \ddot{\phi}(t), \\ y(t) &= \phi(t) + \eta(t), \end{aligned} \right\} \quad (5)$$

based on the measured output $y(t)$ only. The signal $\ddot{\phi}(t)$ is unknown and should be considered as a perturbation. Designing the state estimates $(\hat{x}_1(t), \hat{x}_2(t))$ using the *supertwist observer*, we may conclude that $\hat{x}_2(t)$ may be considered as an estimate of $\dot{\phi}(t)$:

$$x_2(t) \simeq \dot{\phi}(t)$$

Super-twist differentiator with low-pass filter

$$\frac{d}{dt}\hat{x}_1(t) = \hat{x}_2(t) - \alpha \|\phi(t) - \hat{x}_1(t)\|^{1/2} \text{SIGN}(\hat{x}_1(t) - y(t)),$$

$$\frac{d}{dt}\hat{x}_2(t) = -\beta \text{SIGN}(\hat{x}_1(t) - y(t)), \quad |\dot{\phi}(t)| \leq \beta, \quad \alpha > 4\beta,$$

and low-pass filter:

$$\mu \dot{v}(t) + v(t) = \hat{x}_2(t), \quad \mu = 0.01,$$

(6)

so that,

$$v(t) \simeq \dot{\phi}(t).$$